

A Well-conditioned Weak Coupling of Boundary Element and High-order Finite Element Methods for Time-harmonic Electromagnetic Scattering

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Outline

Introduction

Wave Propagation Model
Standard Approaches

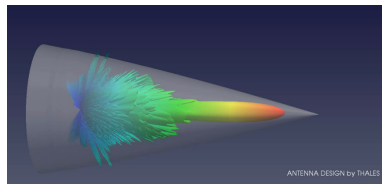
Strong FEM-BEM Coupling

Weak FEM-BEM Coupling

Numerical Results

Applications

Conclusion and Perspectives



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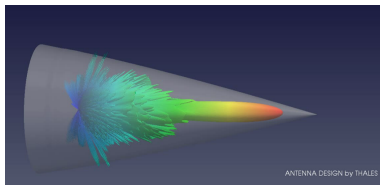
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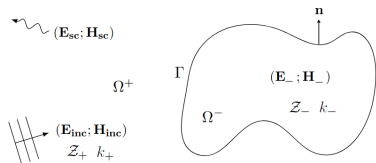
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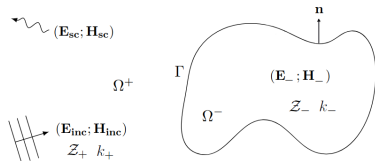
Electromagnetic Scattering Problem



Electromagnetic Scattering Problem

Incident plane wave

$$\mathbf{E}_{\text{inc}} = (e^{ik_+z}; 0; 0)^T$$



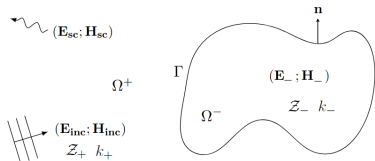
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The total electromagnetic field in Ω_+

$$(\mathbf{E}_+; \mathbf{H}_+) = (\mathbf{E}_{\text{inc}}; \mathbf{H}_{\text{inc}}) + (\mathbf{E}_{\text{sc}}; \mathbf{H}_{\text{sc}})$$



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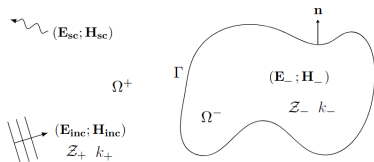
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$$\text{curl } \mathbf{E} - k \nabla \times \mathbf{H} = \mathbf{0}$$

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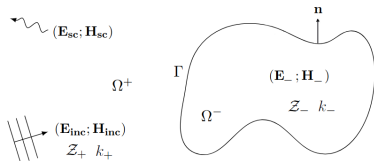
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Silver-Müller radiation condition

$$\nabla \times \mathbf{H}_{\text{sc}} - \frac{\mathbf{x}}{r} \times \nabla \times \mathbf{E}_{\text{sc}} = O(r^{-2})$$



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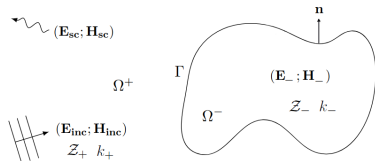
$$\nabla \times \mathbf{H}_{\text{sc}} - \frac{\mathbf{x}}{r} \times \nabla \times \mathbf{E}_{\text{sc}} = O(r^{-2})$$

Transmission conditions on Γ

$$\mathbf{E}_{j\Gamma} \cdot \mathbf{n} = \mathbf{E}_{\text{sc}j\Gamma} \cdot \mathbf{n} + \mathbf{E}_{\text{inc}j\Gamma} \cdot \mathbf{n}$$

$$\mathbf{H}_{j\Gamma} \cdot \mathbf{n} = \mathbf{H}_{\text{sc}j\Gamma} \cdot \mathbf{n} + \mathbf{H}_{\text{inc}j\Gamma} \cdot \mathbf{n}$$

with \mathbf{n} the outward pointing normal on



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Surface integral equations for the exterior domain: exact at the continuous level and adapted to homogeneous domain.

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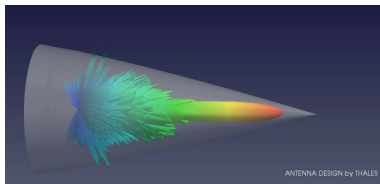
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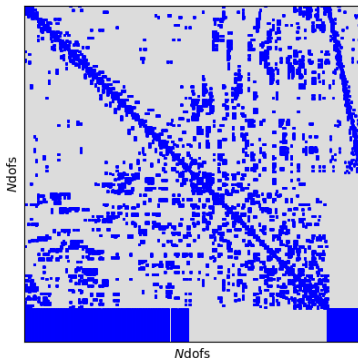
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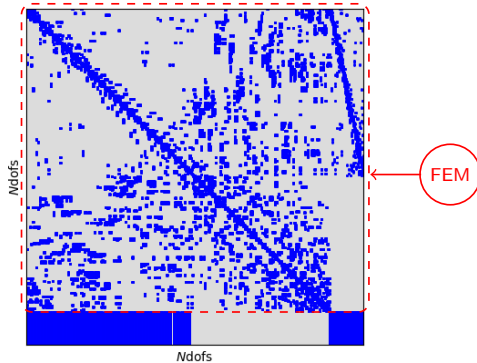


Strong Coupling, a Standard Resolution Method



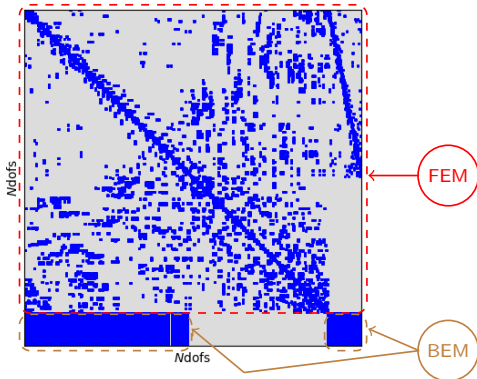
Matrix resulting from the coupling of **variational formulation** for Ω and an **integral equation** for Ω_+ in one unique formulation.

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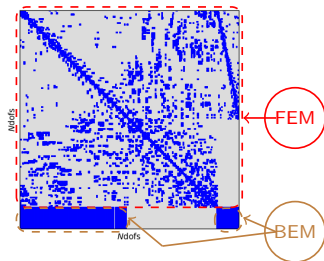


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Motivations for a New Method

Difficulty for classical iterative methods

Strong FEM-BEM leads to a matrix with sparse and dense blocks.



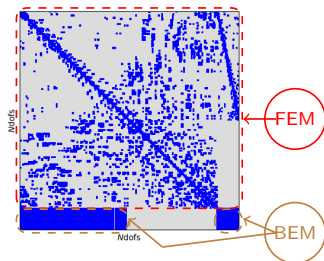
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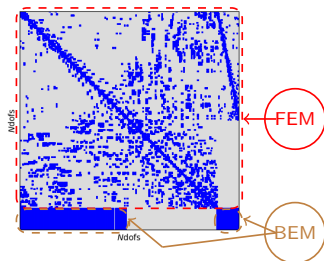
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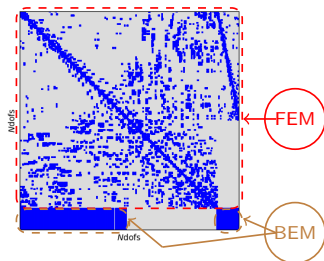
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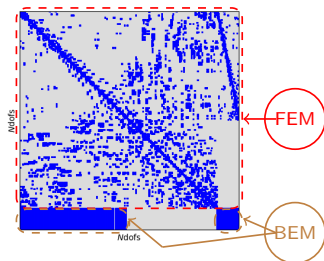
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A simple solution to all these problems

Domain decomposition between the interior domain and the exterior domain.

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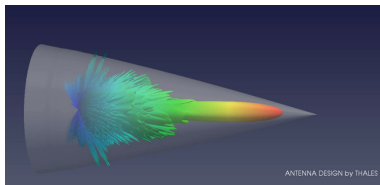
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What is the Weak Coupling?

It is a Schwarz-like method: reformulate the transmission conditions on Γ

$$\begin{aligned}(\mathbf{H}_{j\Gamma} \cdot \mathbf{n}) + \mathbf{T}(\mathbf{E}_{j\Gamma} \cdot \mathbf{n}) &= (\mathbf{H}_{+j\Gamma} \cdot \mathbf{n}) + \mathbf{T}(\mathbf{E}_{+j\Gamma} \cdot \mathbf{n}) \\ (\mathbf{H}_{+j\Gamma} \cdot \mathbf{n}) - \mathbf{T}_+(\mathbf{E}_{+j\Gamma} \cdot \mathbf{n}) &= (\mathbf{H}_{j\Gamma} \cdot \mathbf{n}) - \mathbf{T}_+(\mathbf{E}_{j\Gamma} \cdot \mathbf{n})\end{aligned}$$

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Unknowns of the weak coupling

$$\mathbf{g} = (\mathbf{H}_{j\Gamma} \quad \mathbf{n}) - \mathbf{T} (\mathbf{E}_{j\Gamma} \quad \mathbf{n})$$

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Unknowns of the weak coupling

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Affine resolution operators (the pre-existing solvers)

$$\mathbf{R} \mathbf{g} = \mathbf{E}_{j\Gamma} \quad \mathbf{n} \text{ (FEM solver)} \text{ and } \mathbf{R}_+ \mathbf{g} = \mathbf{E}_{+j\Gamma} \quad \mathbf{n} \text{ (BEM solver)}$$

where $(\mathbf{E}; \mathbf{H})$ are the solutions of the following boundary-value problems:

$$\begin{aligned} \text{curl } \mathbf{E} - k \nabla \times \mathbf{H} &= \mathbf{0}; \text{ in } \Omega \\ \text{curl } \mathbf{H} + k \nabla \times \mathbf{E} &= \mathbf{0}; \text{ in } \Omega \\ (\mathbf{H}_{j\Gamma} \quad \mathbf{n}) - \mathbf{T} (\mathbf{E}_{j\Gamma} \quad \mathbf{n}) &= \mathbf{g}; \text{ on } \Gamma \\ \nabla_{\perp} \cdot \mathbf{H}_{\text{sc}} - \frac{\mathbf{x}}{k \times k} \cdot \nabla \mathbf{E}_{\text{sc}} &= \frac{r!}{r! + 1} (r^{-2}); \end{aligned}$$

The Weak FEM-BEM Coupling

/ Rewriting of the reformulated transmission conditions

The weak FEM-BEM coupling

$$\begin{pmatrix} \mathbf{Id} & \mathbf{S} \end{pmatrix} \begin{pmatrix} \mathbf{g} \\ \mathbf{g}_+ \end{pmatrix} = \begin{pmatrix} \mathbf{0} \\ \mathbf{0} \end{pmatrix}$$

$$\text{with } S_{\pi} = \begin{pmatrix} 0 & \mathbf{S}_+ \\ \mathbf{S} & 0 \end{pmatrix}, \mathbf{S} = \mathbf{Id} - (\mathbf{T} + \mathbf{T}_+)\mathbf{R}$$

Reformulation of the Weak Coupling

Reformulation of the weak FEM-BEM coupling

The weak FEM-BEM coupling can be recast into a linear system:

$$\begin{pmatrix} \mathbf{Id} & A \end{pmatrix} \begin{pmatrix} \mathbf{g} \\ \mathbf{g}_+ \end{pmatrix} = \begin{pmatrix} \mathbf{b} \\ \mathbf{b}_+ \end{pmatrix} \quad (/),$$

where the information about the incident plane wave is contained in the right-hand side. The quantities \mathbf{g} and \mathbf{g}_+ can be interpreted as some exchanged information from Ω_+ to Ω and from Ω to Ω_+ , respectively.

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Continuous approach - The weak FEM-BEM coupling formulation

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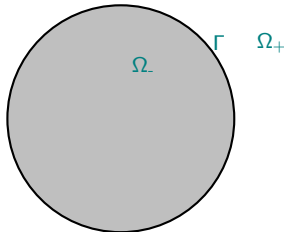
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At each iteration of a **Krylov subspace solver** of (/):



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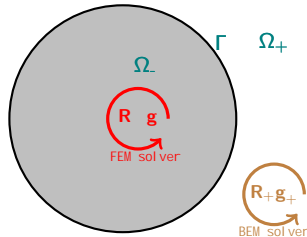
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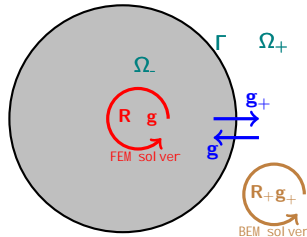
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Continuous approach - The weak **FEM-BEM** coupling formulation

At each iteration of a **Krylov subspace solver** of (//):

1. Solve the **interior problem** and the **exterior problem**.
2. **Update** the interface unknowns \mathbf{g}_+ and \mathbf{g} (using A).



Correctly Choosing the Transmission Operators

The weak coupling can **only be solved iteratively**, typically using the GMRES method.

/ The GMRES convergence of the weak coupling is fundamentally related to the choice of the transmission operators.

Optimal transmission operators for the weak coupling

[Caudron, Geuzaine, Antoine, 2018]

$$\begin{aligned} \mathbf{T} &= \Lambda_{+,k_+;Z_+} \mathbf{S}_+ = \mathbf{0} \\ \mathbf{T}_+ &= \Lambda_{-,k_-;Z_-} \mathbf{S}_- = \mathbf{0} \\ & \quad) \operatorname{Sp}(\mathbf{Id} - \mathbf{A}) = \rho_1 g \end{aligned}$$

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Remarks: Unlike the interior problem (complex **nonlocal** interactions), the solution of the exterior domain is **spatially localized**.

/ Use accurate representation of $\mathbf{T} = \Lambda_{+,k_+;Z_+}$ and rough computation of \mathbf{T}_+ (poor approximation of $\Lambda_{+,k_+;Z_+}$ or $\Lambda_{-,k_-;Z_-}$).

) \mathbf{A} nilpotent (leading fast convergence of the GMRES)

Approximating The **MtE** Operators

What about the practical side?

In practice, evaluating **MtE** operators leads to high computational costs.
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Low order approximations

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Low order approximations

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Padé-localized square-root approximations [El Bouajaji, Antoine, Geuzaine, 2014]

$$\frac{1}{Z} \left(C_0 + \sum_{l=1}^p A_l \right) \mathbf{r}_\Gamma \left(\frac{1}{k^2} \text{div}_\Gamma \right) \text{curl}_\Gamma \left(\frac{1}{k^2} \text{curl}_\Gamma \right) \text{Id} + B_l \mathbf{r}_\Gamma \left(\frac{1}{k^2} \text{div}_\Gamma \right) \text{rot}_\Gamma \left(\frac{1}{k^2} \text{rot}_\Gamma \right) \text{Id} - \text{curl}_\Gamma \left(\frac{1}{k^2} \text{curl}_\Gamma \right) (\text{Id} - \mathbf{n})$$

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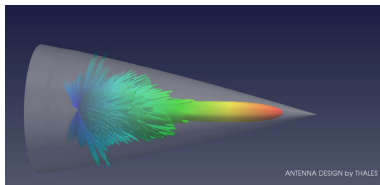
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Numerical Results

FEM solver

GmshFEM,

a newly developed open-source finite element library based on Gmsh

BEM solver

Bempp-cl ,

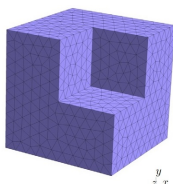
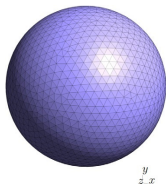
an open-source boundary element library

The transmission operators selected

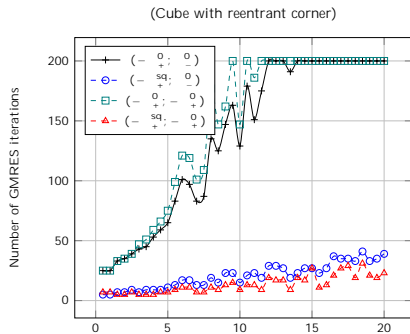
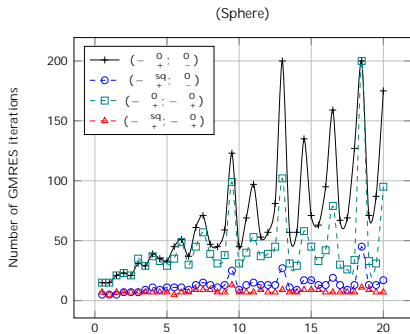
$$(\mathbf{T} ; \mathbf{T}_+)$$

We suppose

$$k = k_+ e^{-kxk^2} \text{ and } Z = Z_+ e^{kxk^2} \text{ with } Z \in \mathbb{R}_+ \text{ and } Z_+ = Z_0$$

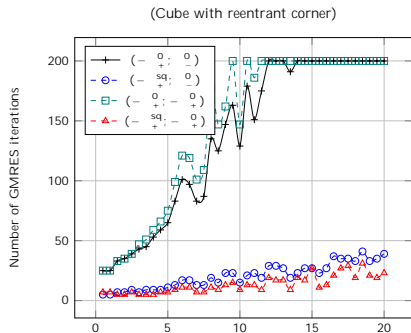
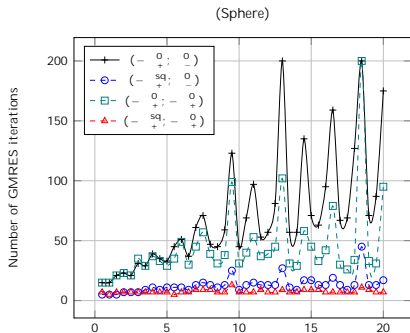


Number Of GMRES Iterations Vs.



5 points per wavelength and $k_+ = 1$

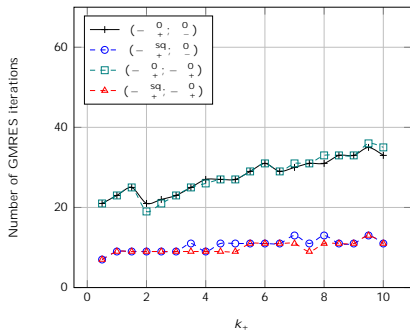
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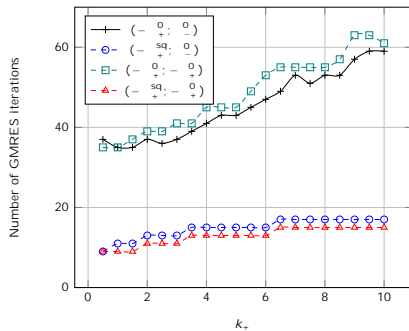
5 points per wavelength and $k_+ = 1$
 ! Superior iterative performance when $\mathbf{T}_+ = \mathbf{\Lambda}_{+;k_+;Z_+}^0$

Number Of GMRES Iterations Vs. k_+

(Sphere)



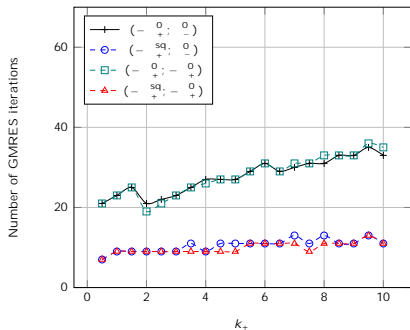
(Cube with reentrant corner)



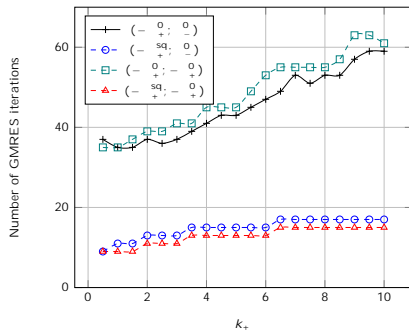
5 points per wavelength, $\Delta x = 2$

Number Of GMRES Iterations Vs. k_+

(Sphere)



(Cube with reentrant corner)

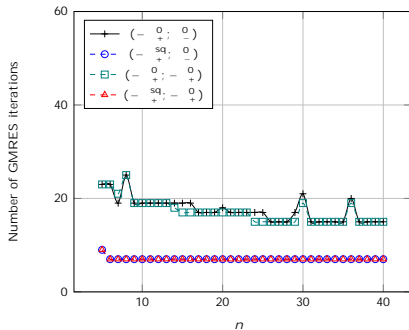


5 points per wavelength, $\nu = 2$

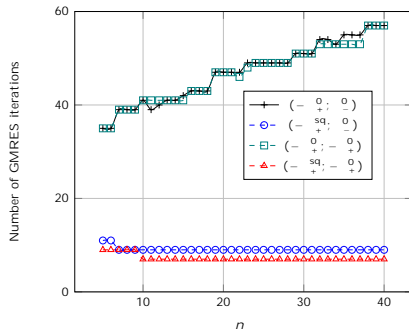
! $(\Lambda_{+;k_+;Z_+}^{sq;Np;p}; \Lambda_{+;k_+;Z_+}^0)$ leads to the **lowest dependency** of the GMRES iterations with respect to k_+

Influence Of Mesh Refinement

(Sphere)

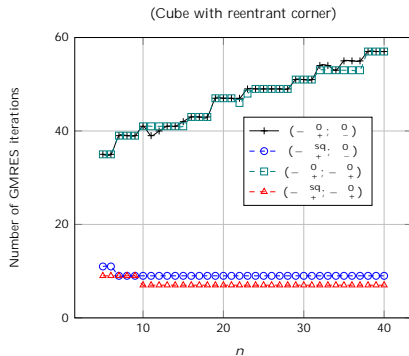
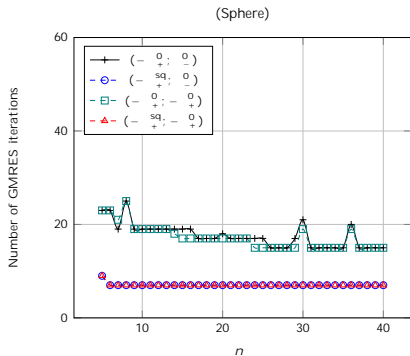


(Cube with reentrant corner)



$$= 2 \text{ and } k_+ = 1$$

Influence Of Mesh Refinement



$$= 2 \text{ and } k_+ = 1$$

! Convergence clearly **deteriorates** with the pairs $(\Lambda_{+;k_+;Z_+}^0; \Lambda_{;k_-;Z_-}^0)$

Accuracy of the weak FEM-BEM coupling

Relative differences in $L_t^2(\Gamma)$ -norm between the strong and the weak FEM-BEM coupling electric/magnetic currents

$$\varrho_{\mathbf{H}} : h_{j\Gamma} \mathbf{n} = \frac{k_{\mathbf{H}} : h_{j\Gamma} \mathbf{n} \mathbf{H}_{j\Gamma}^{\text{Ref}} \mathbf{n} k_{L_t^2(\Gamma_h)}}{k_{\mathbf{H}} : h_{j\Gamma} \mathbf{n} \mathbf{H}_{j\Gamma}^{\text{Ref}} \mathbf{n} k_{L_t^2(\Gamma_h)}};$$

$$\varrho_{\mathbf{E}} : h_{j\Gamma} \mathbf{n} = \frac{k_{\mathbf{E}} : h_{j\Gamma} \mathbf{n} \mathbf{E}_{j\Gamma}^{\text{Ref}} \mathbf{n} k_{L_t^2(\Gamma_h)}}{k_{\mathbf{E}} : h_{j\Gamma} \mathbf{n} \mathbf{E}_{j\Gamma}^{\text{Ref}} \mathbf{n} k_{L_t^2(\Gamma_h)}};$$

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k_+		$e_{\mathbf{E}} ; h_{j\Gamma} \mathbf{n}$	$e_{\mathbf{H}} ; h_{j\Gamma} \mathbf{n}$
1	2	9.9%	0.8%
2	2	7.5%	0.8%
1	3	5.7%	4.9%
1	4	2.9%	1.0%

$e_{\mathbf{E}} ; h_{j\Gamma} \mathbf{n}$ and $e_{\mathbf{H}} ; h_{j\Gamma} \mathbf{n}$ for the sphere and for different k_+ and $(n = 10)$

Outline

Introduction

Wave Propagation Model
Standard Approaches

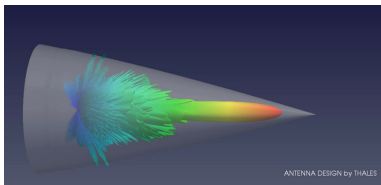
Strong FEM-BEM Coupling

Weak FEM-BEM Coupling

Numerical Results

Applications

Conclusion and Perspectives



Applications

FEM solver

GmshFEM

BEM solver

Antenna Design (AD) coupled with the H-Matrix library Hi-BoX,
the Thales internally developed code

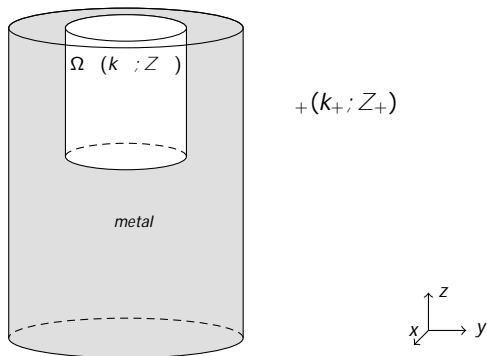
Validation

The test cases were validated using AD coupled with Hi-BoX

The transmission operators selected

$$(\mathbf{T} ; \mathbf{T}_+) = (\mathbf{\Lambda}_+^{\text{sq}} ; \mathbf{\Lambda}_+^0)$$

Partially coated domain



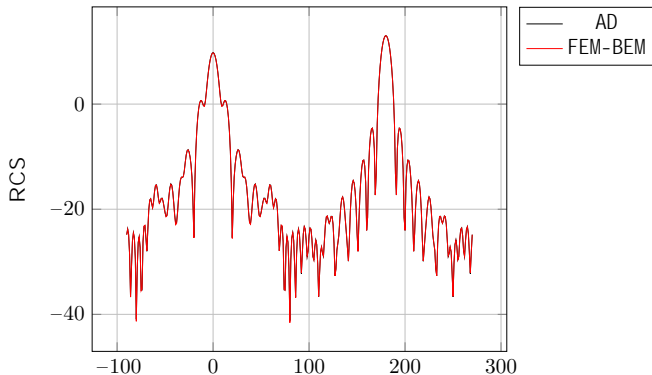
Incident plane wave linearly polarized along z

Frequency: 10[GHz]

$$= (0.895 \quad 0.021) \quad 0, \quad = 0,$$

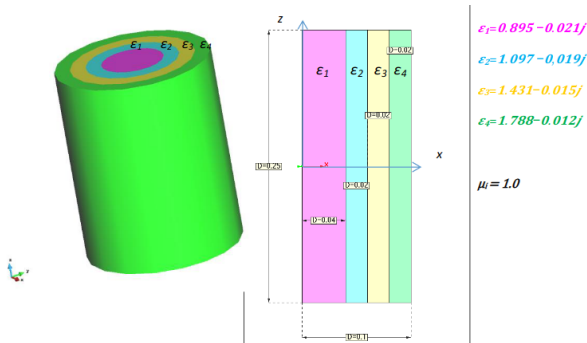
$$+ = 0, \quad + = 0$$

The bistatic RCS in plane $y = 0$



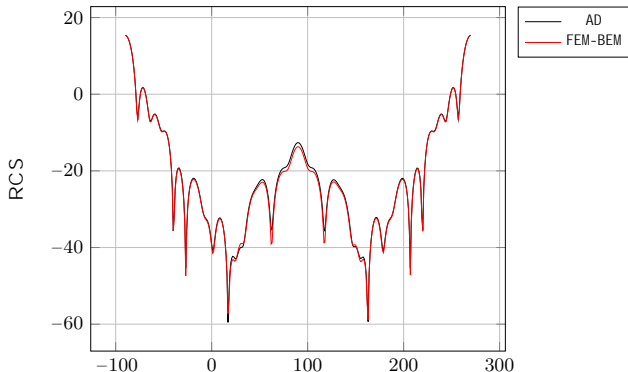
Good convergence of GMRES in 11 iterations

Multilayer Dielectric Cylinder



Incident plane wave linearly polarized along x
Frequency: 5[GHz]

The bistatic RCS in plane $y = 0$



Good convergence of GMRES in 15 iterations

A K/KA Dual Band Polarizer

A K/KA Dual Band Polarizer

We compute the RHCP gain and the LHCP gain in the yz plane defined by

$$RHCP(\theta; 90) = 20 \log \left(\frac{1}{\sqrt{2}} (E_{sc; \theta}^1(\theta; 90) + E_{sc; \theta}^1(\theta; 90)) \right);$$

$$LHCP(\theta; 90) = 20 \log \left(\frac{1}{\sqrt{2}} (E_{sc; \theta}^1(\theta; 90) - E_{sc; \theta}^1(\theta; 90)) \right);$$

where we denote the components of the far-field by $E_{sc; \theta}^1$ and $E_{sc; \theta}^1$;

A K/KA Dual Band Polarizer

A K/KA Dual Band Polarizer

The polarizer is tested with two linearly polarized rectangular horns, one for each band (20.2[GHz] and 30[GHz])

This problem can be challenging due to the rather small thickness and intricacies of the polarizer

For more information: P. Naseri et al, *Dual-Band Dual-Linear-to-Circular Polarization Converter in Transmission Mode Application to K/Ka -Band Satellite Communications*, in IEEE, 2018.

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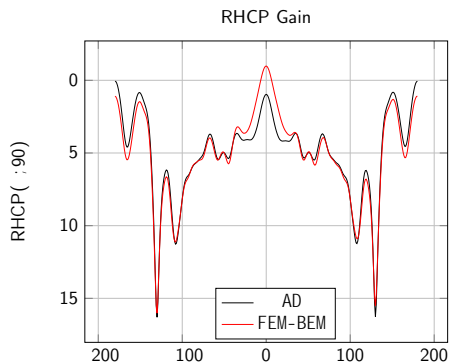
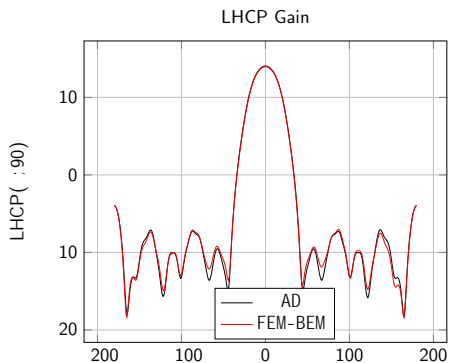
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A K/Ka Dual Band Polarizer

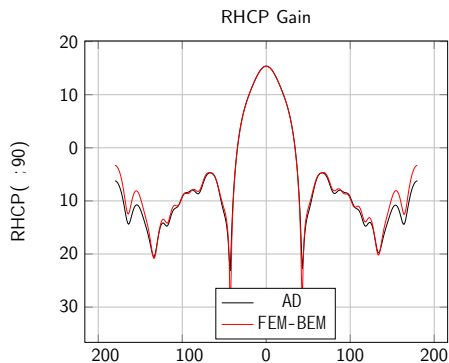
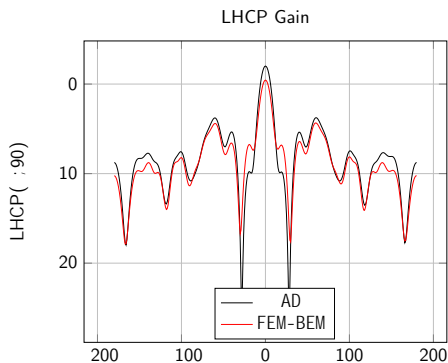
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Good convergence of GMRES in 15 iterations



Good convergence of GMRES in 17 iterations

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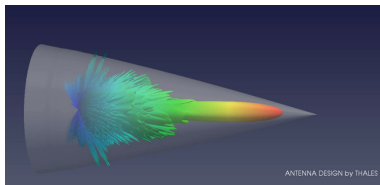
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Weak FEM-BEM Coupling

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Features of the new weak FEM-BEM coupling

The convergence rate is **slightly dependent** on the geometry configuration, the frequency k , the mesh refinement and the contrast between the two subdomains.

Allows to reuse optimized pre-existing solvers.

For a relevant accuracy on the far-field, the number of iterations is very small and stable (typically about 15).

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Perspectives

DDM for FEM part.

Perspectives

DDM for FEM part.

(a) Concentric partition

(b) Partition with corners

Perspectives

	Concentric partition	Partition with junctions
GMRES iterations	9	30
$\epsilon_{\mathbf{E}} : h_{j\Gamma} \quad \mathbf{n}$	1.8%	3.8%
$\epsilon_{\mathbf{H}} : h_{j\Gamma} \quad \mathbf{n}$	0.5%	2.6%

I. Badia, C. Caudron, X. Antoine and C. Geuzaine. *A well-conditioned weak coupling of boundary element and high-order finite element methods for time-harmonic electromagnetic scattering by inhomogeneous objects*, to be published in SIAM Journal on Scientific Computing, 2022

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Thank you for your attention !

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