

# A Well-conditioned Weak Coupling of Boundary Element and High-order Finite Element Methods for Time-harmonic Electromagnetic Scattering

I. Badia<sup>1,2,3</sup>   X. Antoine<sup>1</sup>   C. Geuzaine<sup>2</sup>   S. Nosal<sup>3</sup>  
J-P. Martinaud<sup>3</sup>

<sup>1</sup>Institut Élie Cartan de Lorraine, Université de Lorraine

<sup>2</sup>Montefiore Institute, Université de Liège

<sup>3</sup>Thales Defense Mission Systems

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# Outline

## Introduction

Wave Propagation Model  
Standard Approaches

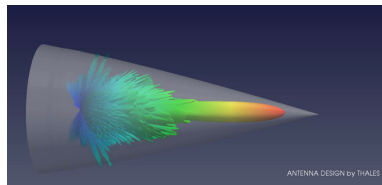
## Strong FEM-BEM Coupling

## Weak FEM-BEM Coupling

## Numerical Results

## Applications

## Conclusion and Perspectives



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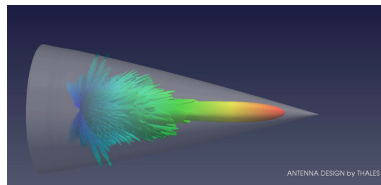
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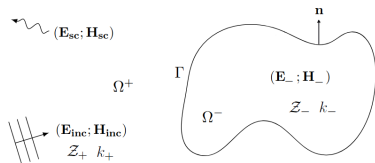
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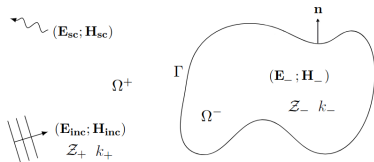
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## Incident plane wave

$$\mathbf{E}_{\text{inc}} = (e^{ik_+ \cdot z}, 0, 0)^T$$



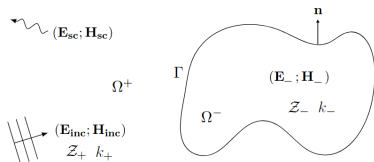
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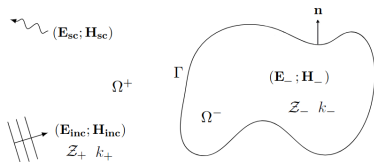
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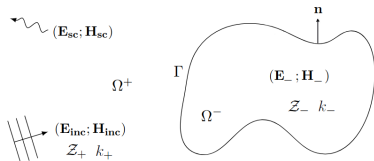
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## Silver-Müller radiation condition

$$\mathcal{Z}_+ \mathbf{H}_{\text{sc}} \times \frac{\mathbf{x}}{||\mathbf{x}||} - \mathbf{E}_{\text{sc}} = \mathcal{O}(r^{-2})$$
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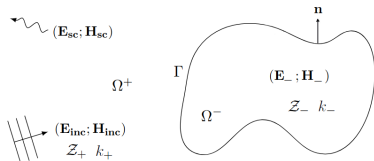
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## Transmission conditions on $\Gamma$

$$\mathbf{E}_{-|_{\Gamma}} \times \mathbf{n} = \mathbf{E}_{\text{sc}|_{\Gamma}} \times \mathbf{n} + \mathbf{E}_{\text{inc}|_{\Gamma}} \times \mathbf{n}$$

$$\mathbf{H}_{-|_{\Gamma}} \times \mathbf{n} = \mathbf{H}_{\text{sc}|_{\Gamma}} \times \mathbf{n} + \mathbf{H}_{\text{inc}|_{\Gamma}} \times \mathbf{n}$$

with  $\mathbf{n}$  the outward pointing normal on  $\Gamma$



# Standard Approaches

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→ Two standard approaches to overcome this difficulty:

- Truncation methods (PML or ABC): approximate the scattering problems at the continuous level.
- **Surface integral equations for the exterior domain**: exact at the continuous level and adapted to homogeneous domain.

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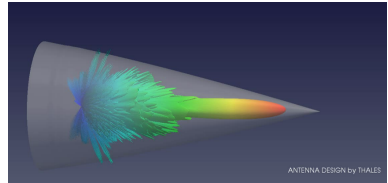
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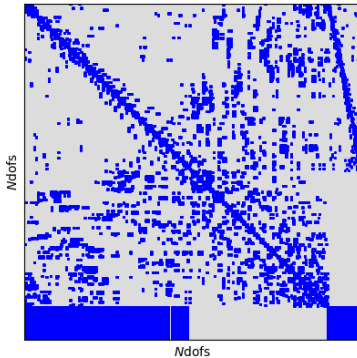
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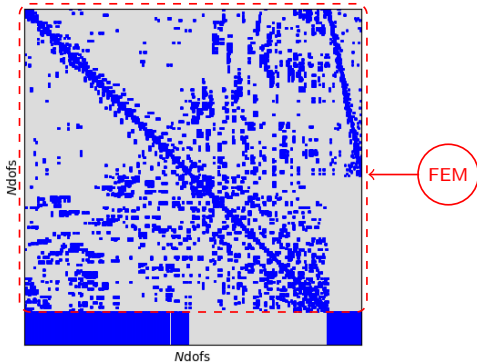


# Strong Coupling, a Standard Resolution Method



Matrix resulting from the coupling of **variational formulation** for  $\Omega_-$  and an **integral equation** for  $\Omega_+$  in one unique formulation.

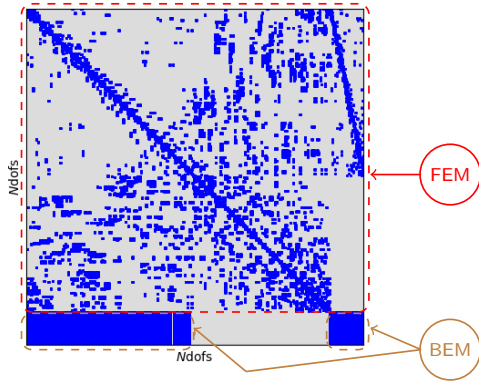
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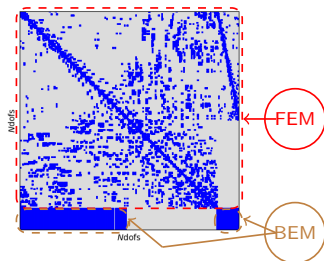


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## Difficulty for classical iterative methods

- Strong FEM-BEM leads to a matrix with sparse and dense blocks.



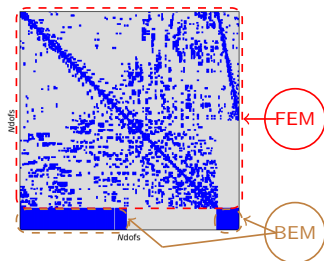
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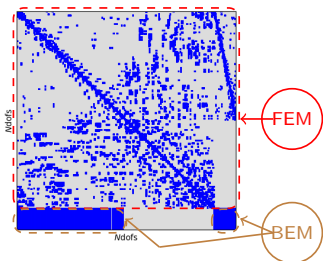
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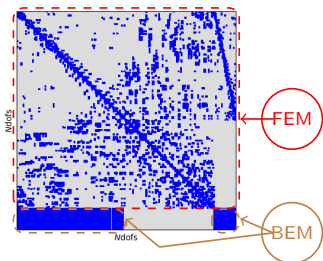
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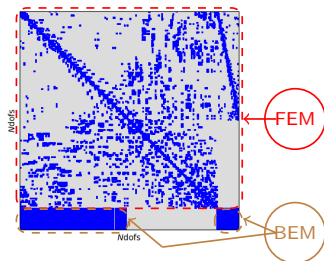
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## A simple solution to all these problems

**Domain decomposition** between the interior domain and the exterior domain.

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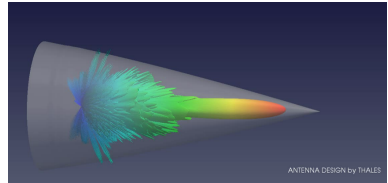
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# What is the Weak Coupling?

**It is a Schwarz-like method: reformulate the transmission conditions on  $\Gamma$**

$$\begin{aligned}(\mathbf{H}_{-|\Gamma} \times \mathbf{n}) + \mathbf{T}_{-}(\mathbf{E}_{-|\Gamma} \times \mathbf{n}) &= (\mathbf{H}_{+|\Gamma} \times \mathbf{n}) + \mathbf{T}_{-}(\mathbf{E}_{+|\Gamma} \times \mathbf{n}) \\(\mathbf{H}_{+|\Gamma} \times \mathbf{n}) - \mathbf{T}_{+}(\mathbf{E}_{+|\Gamma} \times \mathbf{n}) &= (\mathbf{H}_{-|\Gamma} \times \mathbf{n}) - \mathbf{T}_{+}(\mathbf{E}_{-|\Gamma} \times \mathbf{n})\end{aligned}$$



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$$\mathbf{g}_{\pm} = (\mathbf{H}_{\pm|\Gamma} \times \mathbf{n}) \mp \mathbf{T}_{\pm}(\mathbf{E}_{\pm|\Gamma} \times \mathbf{n})$$

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**Affine resolution operators (the pre-existing solvers)**

$$\mathbf{R}_{-}\mathbf{g} = \mathbf{E}_{-|\Gamma} \times \mathbf{n} \text{ (FEM solver)} \text{ and } \mathbf{R}_{+}\mathbf{g} = \mathbf{E}_{+|\Gamma} \times \mathbf{n} \text{ (BEM solver)}$$

where  $(\mathbf{E}_{\pm}; \mathbf{H}_{\pm})$  are the solutions of the following boundary-value problems:

$$\begin{aligned}\operatorname{curl} \mathbf{E}_{\pm} - \iota k_{\pm} \mathcal{Z}_{\pm} \mathbf{H}_{\pm} &= \mathbf{0}, \text{ in } \Omega_{\pm} \\ \operatorname{curl} \mathbf{H}_{\pm} + \iota k_{\pm} \mathcal{Z}_{\pm}^{-1} \mathbf{E}_{\pm} &= \mathbf{0}, \text{ in } \Omega_{\pm} \\ (\mathbf{H}_{\pm|\Gamma} \times \mathbf{n}) \mp \mathbf{T}_{\pm}(\mathbf{E}_{\pm|\Gamma} \times \mathbf{n}) &= \mathbf{g}, \text{ on } \Gamma \\ \mathcal{Z}_{+} \mathbf{H}_{\text{sc}} \times \frac{\mathbf{x}}{\|\mathbf{x}\|} - \mathbf{E}_{\text{sc}} &= \mathcal{O}(r^{-2}), \text{ as } r \rightarrow +\infty.\end{aligned}$$

# The Weak FEM-BEM Coupling

→ Rewriting of the reformulated transmission conditions

## The weak FEM-BEM coupling

$$(\mathbf{Id} - \mathcal{S}_\pi) \begin{pmatrix} \mathbf{g}_- \\ \mathbf{g}_+ \end{pmatrix} = \begin{pmatrix} \mathbf{0} \\ \mathbf{0} \end{pmatrix}$$

$$\text{with } \mathcal{S}_\pi = \begin{pmatrix} 0 & \mathbf{S}_+ \\ \mathbf{S}_- & 0 \end{pmatrix}, \mathbf{S}_\pm = \mathbf{Id} \pm (\mathbf{T}_- + \mathbf{T}_+) \mathbf{R}_\pm$$

# Reformulation of the Weak Coupling

## Reformulation of the weak FEM-BEM coupling

The weak FEM-BEM coupling can be recast into a linear system:

$$(\text{Id} - \mathcal{A}) \begin{pmatrix} \mathbf{g}_- \\ \mathbf{g}_+ \end{pmatrix} = \begin{pmatrix} \mathbf{b}_- \\ \mathbf{b}_+ \end{pmatrix} (\clubsuit),$$

where the information about the incident plane wave is contained in the right-hand side. The quantities  $\mathbf{g}_-$  and  $\mathbf{g}_+$  can be interpreted as some exchanged information from  $\Omega_+$  to  $\Omega_-$  and from  $\Omega_-$  to  $\Omega_+$ , respectively.

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Continuous approach - The weak **FEM-BEM** coupling formulation

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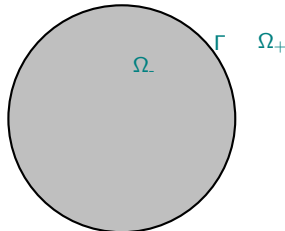
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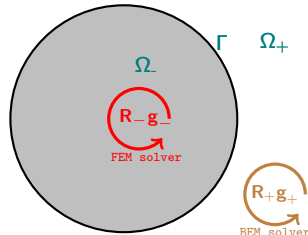
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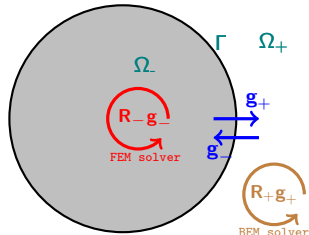
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At each iteration of a **Krylov subspace solver** of ( $\clubsuit$ ):

1. Solve the **interior problem** and the **exterior problem**.
2. **Update** the interface unknowns  $\mathbf{g}_+$  and  $\mathbf{g}_-$  (using  $\mathcal{A}$ ).





# Correctly Choosing the Transmission Operators

The weak coupling can **only be solved iteratively**, typically using the GMRES method.

→ The GMRES convergence of the weak coupling is fundamentally related to the choice of the transmission operators.

## Optimal transmission operators for the weak coupling

[Caudron, Geuzaine, Antoine, 2018]

$$\begin{aligned} \mathbf{T}_- &= -\mathbf{\Lambda}_{+,k_+,Z_+} \Rightarrow \tilde{\mathbf{S}}_+ = 0 \\ \mathbf{T}_+ &= \mathbf{\Lambda}_{-,k_-,Z_-} \Rightarrow \tilde{\mathbf{S}}_- = 0 \\ &\Rightarrow \textcolor{red}{Sp}(\textcolor{red}{Id} - \textcolor{red}{\mathcal{A}}) = \{1\} \end{aligned}$$

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Remarks: Unlike the interior problem (complex **nonlocal** interactions), the solution of the exterior domain is **spatially localized**.

→ Use accurate representation of  $\mathbf{T}_- = -\mathbf{\Lambda}_{+,k_+,Z_+}$  and rough computation of  $\mathbf{T}_+$  ( $\approx$  poor approximation of  $-\mathbf{\Lambda}_{+,k_+,Z_+}$  or  $\mathbf{\Lambda}_{-,k_-,Z_-}$ ).

⇒  $\mathcal{A}$  nilpotent (leading fast convergence of the GMRES)

# Approximating The **MtE** Operators

## What about the practical side?

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$$\Lambda_{\pm, k_{\pm}, \mathcal{Z}_{\pm}}^0 = \mp \frac{1}{\mathcal{Z}_{\pm}} (\text{Id} \times \mathbf{n})$$

### Padé-localized square-root approximations [El Bouajaji, Antoine, Geuzaine, 2014]

$$\begin{aligned} \Lambda_{\pm, k_{\pm}, \mathcal{Z}_{\pm}}^{sq, N_p, \theta_p} = \\ \mp \frac{1}{\mathcal{Z}_{\pm}} \left( C_0 + \sum_{l=1}^{N_p} A_l \left( \nabla_{\Gamma} \left( \frac{1}{k_{\epsilon}^2} \text{div}_{\Gamma} \right) - \text{curl}_{\Gamma} \left( \frac{1}{k_{\epsilon}^2} \text{curl}_{\Gamma} \right) \right) \left( \text{Id} + B_l \left( \nabla_{\Gamma} \left( \frac{1}{k_{\epsilon}^2} \text{div}_{\Gamma} \right) - \text{rot}_{\Gamma} \left( \frac{1}{k_{\epsilon}^2} \text{rot}_{\Gamma} \right) \right) \right)^{-1} \right)^{-1} \\ \left( \text{Id} - \text{curl}_{\Gamma} \left( \frac{1}{k_{\epsilon}^2} \text{curl}_{\Gamma} \right) \right) (\text{Id} \times \mathbf{n}) \end{aligned}$$

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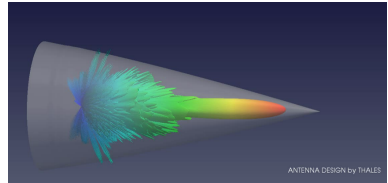
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# Numerical Results

## FEM solver

GmshFEM,

a newly developed open-source finite element library based on Gmsh

## BEM solver

Bempp-cl,

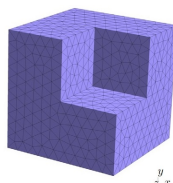
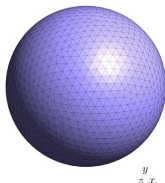
an open-source boundary element library

## The transmission operators selected

$$(\mathbf{T}_-; \mathbf{T}_+)$$

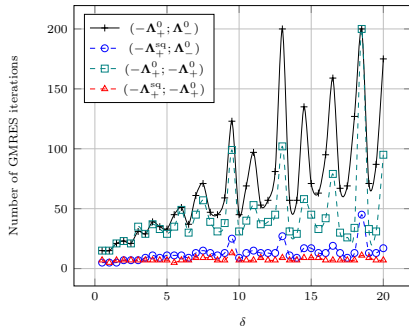
## We suppose

$$k_- = \delta k_+ e^{-\|\mathbf{x}\|^2} \text{ and } \mathcal{Z}_- = \frac{\mathcal{Z}_+}{\delta} e^{\|\mathbf{x}\|^2} \text{ with } \delta \in \mathbb{R}_+^* \text{ and } \mathcal{Z}_+ = \mathcal{Z}_0$$

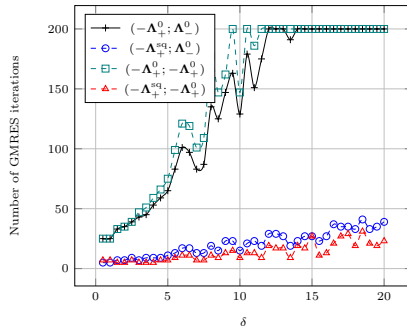


# Number Of GMRES Iterations Vs. $\delta$

(Sphere)



(Cube with reentrant corner)

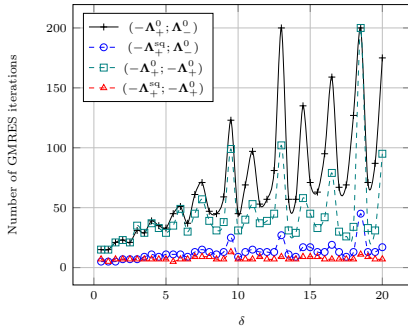


5 points per wavelength and  $k_+ = 1$

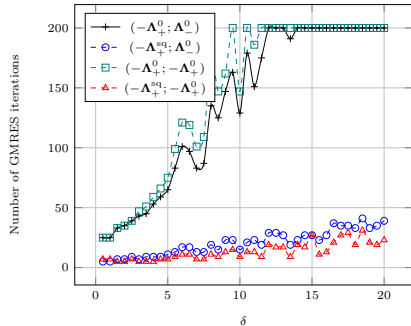


# Number Of GMRES Iterations Vs. $\delta$

(Sphere)



(Cube with reentrant corner)

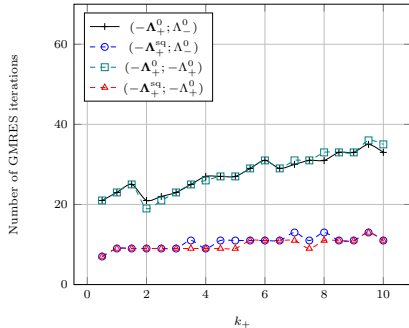


5 points per wavelength and  $k_+ = 1$

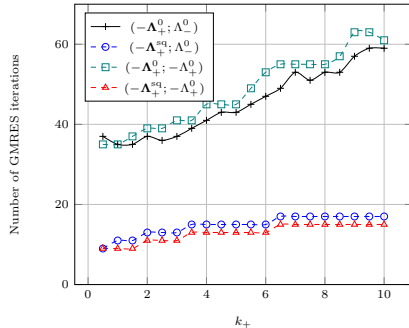
→ **Superior iterative performance** when  $\mathbf{T}_+ = -\Lambda_{+,k_+,\mathcal{Z}_+}^0$

# Number Of GMRES Iterations Vs. $k_+$

(Sphere)



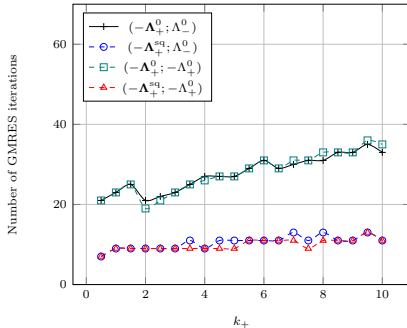
(Cube with reentrant corner)



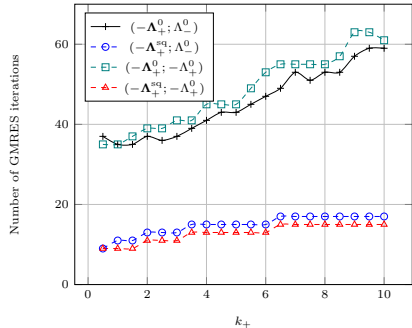
5 points per wavelength,  $\delta = 2$

# Number Of GMRES Iterations Vs. $k_+$

(Sphere)



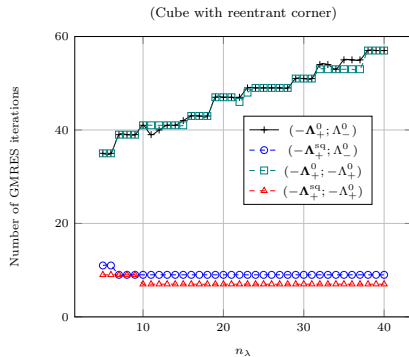
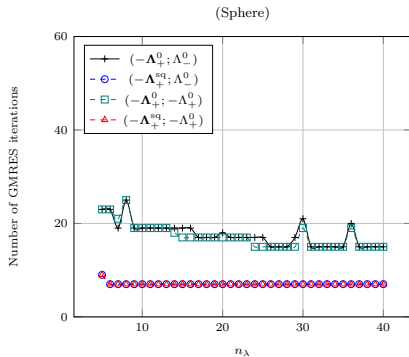
(Cube with reentrant corner)



5 points per wavelength,  $\delta = 2$

$\rightarrow (-\Lambda_{+,k_+,Z_+}^{sq,N_p,\theta_p}; -\Lambda_{+,k_+,Z_+}^0)$  leads to the **lowest dependency** of the GMRES iterations with respect to  $k_+$

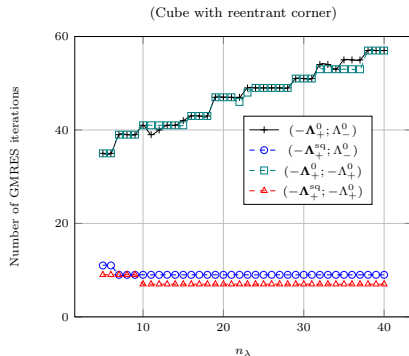
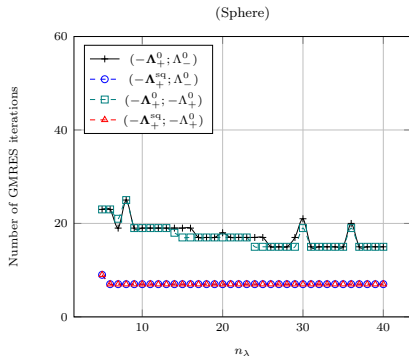
# Influence Of Mesh Refinement



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$$\delta = 2 \text{ and } k_+ = 1$$

# Influence Of Mesh Refinement



$$\delta = 2 \text{ and } k_+ = 1$$

→ Convergence clearly **deteriorates** with the pairs  $(-\Lambda_{+,k_+,z_+}^0; \mp \Lambda_{\pm,k_\pm,z_\pm}^0)$

# Accuracy of the weak FEM-BEM coupling

**Relative differences in  $L_t^2(\Gamma)$ -norm between the strong and the weak FEM-BEM coupling electric/magnetic currents**

$$e_{\mathbf{H}_{-,h|\Gamma} \times \mathbf{n}} = \frac{\|\mathbf{H}_{-,h|\Gamma} \times \mathbf{n} - \mathbf{H}_{|\Gamma}^{\text{Ref}} \times \mathbf{n}\|_{L_t^2(\Gamma_h)}}{\|\mathbf{H}_{|\Gamma}^{\text{Ref}} \times \mathbf{n}\|_{L_t^2(\Gamma_h)}},$$

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$k_+$	$\delta$	$e_{\mathbf{E}_{-,h \Gamma} \times \mathbf{n}}$	$e_{\mathbf{H}_{-,h \Gamma} \times \mathbf{n}}$
1	2	9.9%	0.8%
2	2	7.5%	0.8%
1	3	5.7%	4.9%
1	4	2.9%	1.0%

$e_{\mathbf{E}_{-,h|\Gamma} \times \mathbf{n}}$  and  $e_{\mathbf{H}_{-,h|\Gamma} \times \mathbf{n}}$  for the sphere and for different  $k_+$  and  $\delta$  ( $n_\lambda = 10$ )

# Outline

## Introduction

Wave Propagation Model  
Standard Approaches

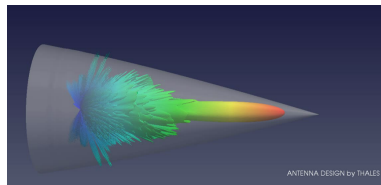
## Strong FEM-BEM Coupling

## Weak FEM-BEM Coupling

## Numerical Results

## Applications

## Conclusion and Perspectives





# Applications

## FEM solver

GmshFEM

## BEM solver

Antenna Design (AD) coupled with the H-Matrix library Hi-BoX,  
the Thales internally developed code

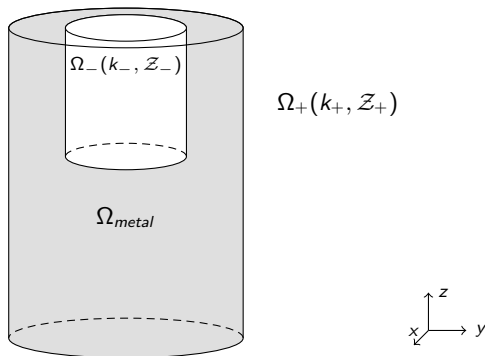
## Validation

The test cases were validated using AD coupled with Hi-BoX

## The transmission operators selected

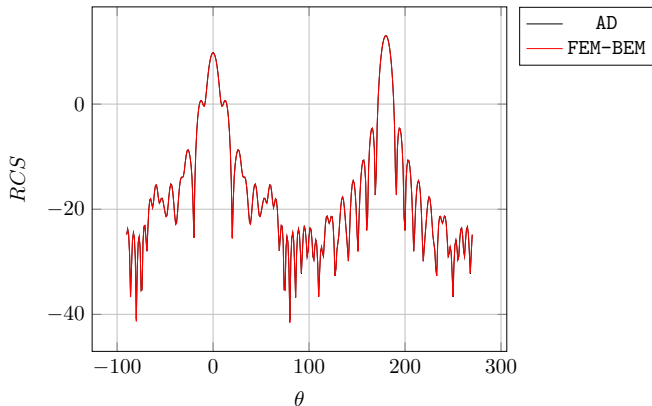
$$(\mathbf{T}_-; \mathbf{T}_+) = (-\mathbf{\Lambda}_+^{\text{sq}}; -\mathbf{\Lambda}_+^0)$$

# Partially coated domain



- Incident plane wave linearly polarized along  $z$
- Frequency:  $10[GHz]$
- $\epsilon_- = (0.895 - i0.021)\epsilon_0$  ,  $\mu_- = \mu_0$ ,
- $\epsilon_+ = \epsilon_0$  ,  $\mu_+ = \mu_0$

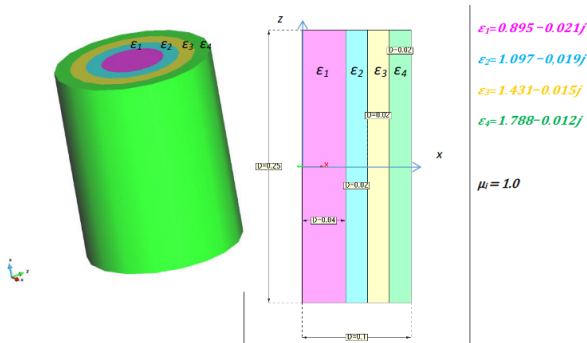
# The bistatic RCS in plane $y = 0$



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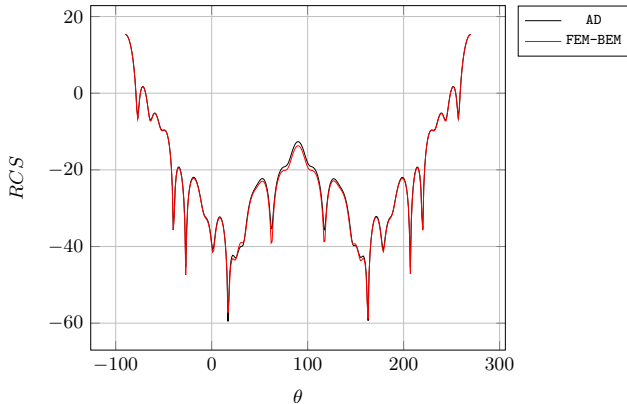
Good convergence of GMRES in 11 iterations

# Multilayer Dielectric Cylinder



- Incident plane wave linearly polarized along  $x$
- Frequency: 5[GHz]

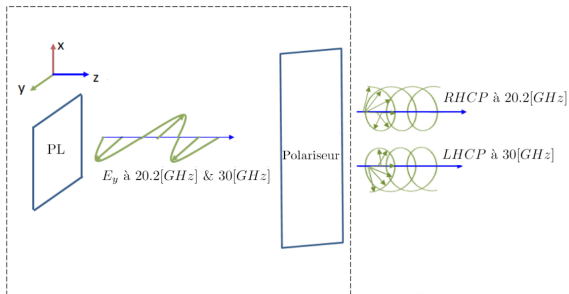
# The bistatic RCS in plane $y = 0$



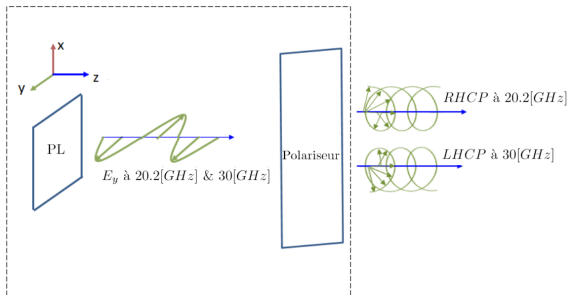
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Good convergence of GMRES in 15 iterations

# A K/KA Dual Band Polarizer



# A K/KA Dual Band Polarizer



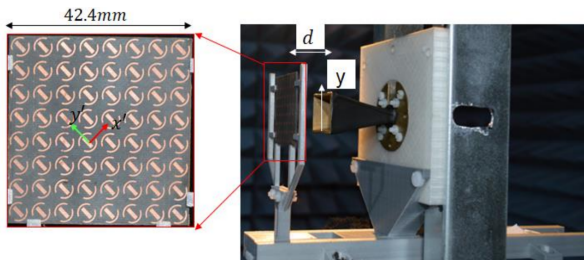
We compute the RHCP gain and the LHCP gain in the  $yz$  plane defined by

$$RHCP(\theta, 90) = 20\log\left(\left|\frac{1}{\sqrt{2}}(E_{sc,\theta}^\infty(\theta, 90) + \iota E_{sc,\phi}^\infty(\theta, 90))\right|\right),$$

$$LHCP(\theta, 90) = 20\log\left(\left|\frac{1}{\sqrt{2}}(E_{sc,\theta}^\infty(\theta, 90) - \iota E_{sc,\phi}^\infty(\theta, 90))\right|\right),$$

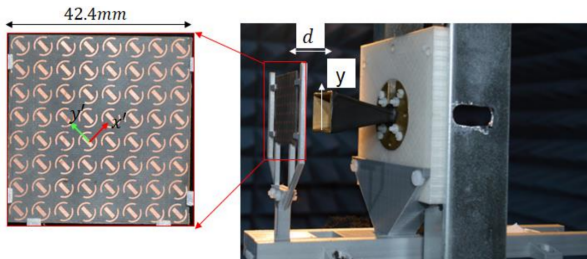
where we denote the components of the far-field by  $E_{sc,\theta}^\infty$  and  $E_{sc,\phi}^\infty$

# A K/KA Dual Band Polarizer



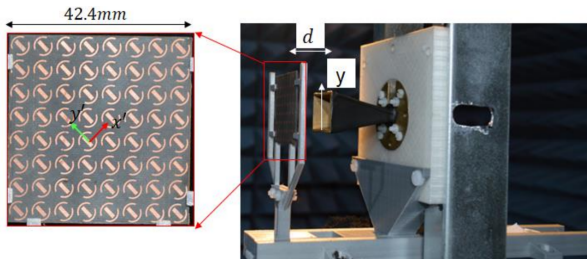


# A K/KA Dual Band Polarizer



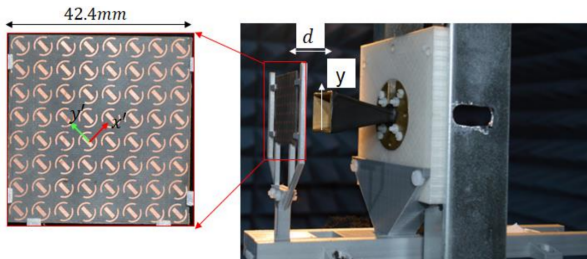
- The polarizer is tested with two linearly polarized rectangular horns, one for each band (20.2[GHz] and 30[GHz])
- This problem can be challenging due to the rather small thickness and intricacies of the polarizer
- For more information: P. Naseri et al, *Dual-Band Dual-Linear-to-Circular Polarization Converter in Transmission Mode Application to K/Ka -Band Satellite Communications*, in IEEE, 2018.

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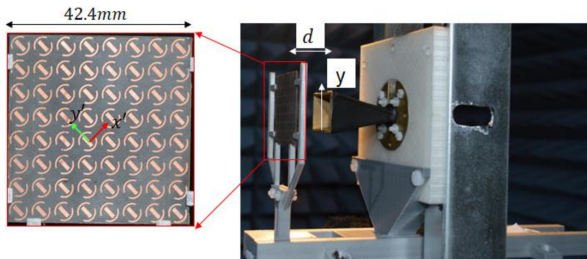
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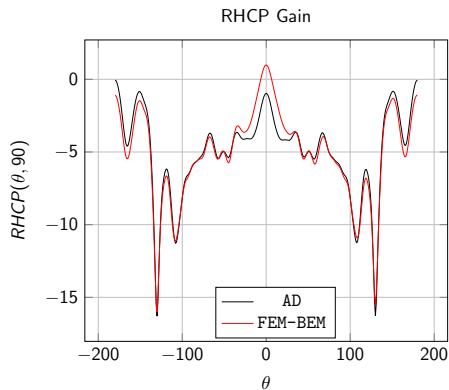
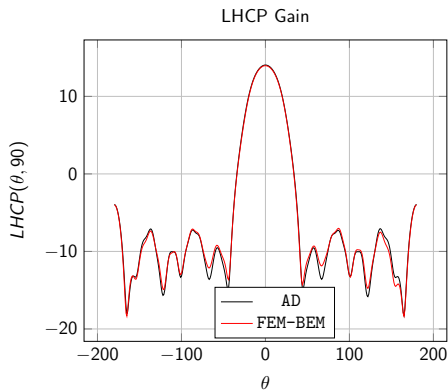


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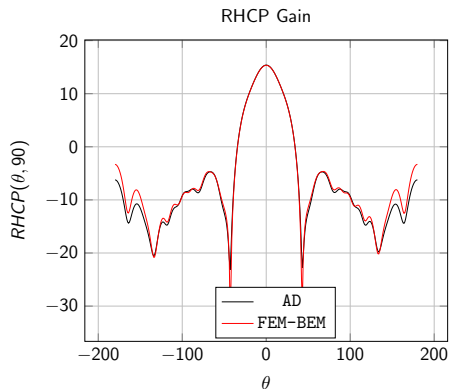
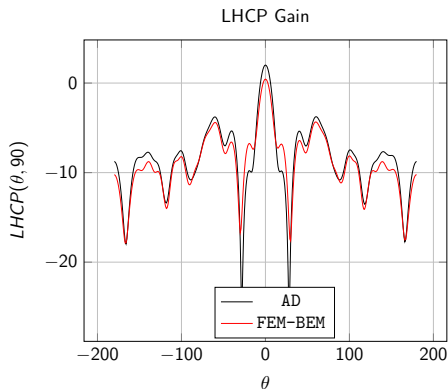


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Good convergence of GMRES in 15 iterations



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Good convergence of GMRES in 17 iterations

# Outline

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Wave Propagation Model  
Standard Approaches

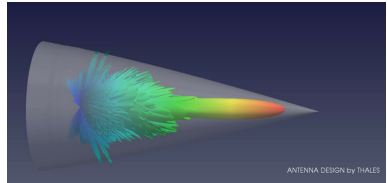
## Strong FEM-BEM Coupling

## Weak FEM-BEM Coupling

## Numerical Results

## Applications

## Conclusion and Perspectives



## Features of the new weak FEM-BEM coupling

- The convergence rate is **slightly dependent** on the geometry configuration, the frequency  $k$ , the mesh refinement and the contrast between the two subdomains.
- Allows to reuse optimized pre-existing solvers.
- For a relevant accuracy on the far-field, the number of iterations is very small and stable (typically about 15).



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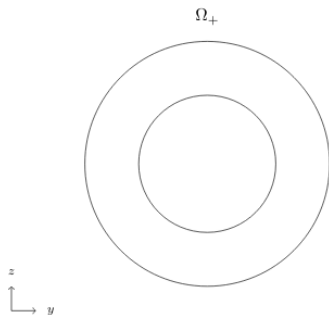
## Perspectives

- DDM for FEM part.

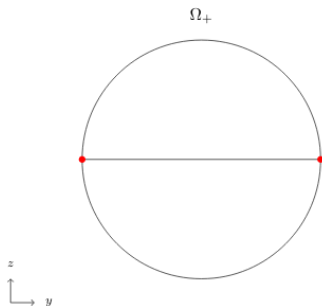
# Perspectives

## Perspectives

- DDM for FEM part.



(a) Concentric partition



(b) Partition with corners

# Perspectives

	Concentric partition	Partition with junctions
GMRES iterations	9	30
$e_{E_{-,h _{\Gamma}}} \times n$	1.8%	3.8%
$e_{H_{-,h _{\Gamma}}} \times n$	0.5%	2.6%

I. Badia, C. Caudron, X. Antoine and C. Geuzaine. *A well-conditioned weak coupling of boundary element and high-order finite element methods for time-harmonic electromagnetic scattering by inhomogeneous objects*, to be published in SIAM Journal on Scientific Computing, 2022

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**Thank you for your attention !**

✉ [ismail.badia@thalesgroup.com](mailto:ismail.badia@thalesgroup.com)